

Assessment of Dynamic Collapse of Container Ship Subjected to Whipping

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Motivation

- Most of the accidents due to whipping load
 - Container ships
 - *MOL Comfort, Napoli, MSC Carla*
- Recent accident of MOL Comfort
 - more interest of whipping effect on the hull girder loadings



MOL Comfort Accident
[<https://goo.gl//velqiC>]

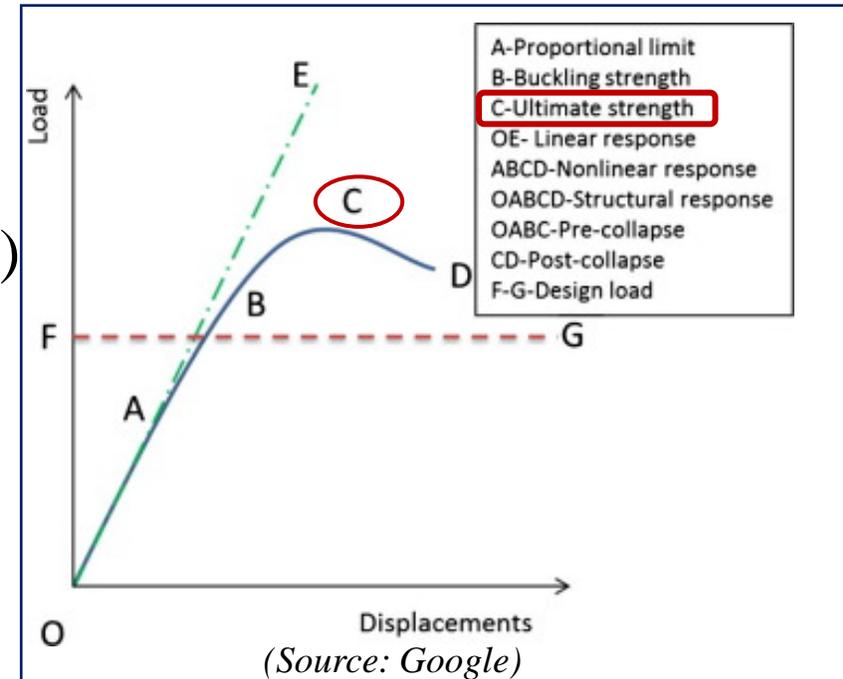
Objectives

- To assess the ultimate strength of 14000 TEU container ship
- To investigate the influence of material strain rate
- To investigate the effect of whipping load on hull girder capacity strength

Introduction

Ultimate strength check → DNV GL class guideline (code-0153)

$$\gamma_S M_{SW} + M_{WV} (\gamma_W + (\gamma_{WH} - \gamma_W) \gamma_{dU}) \leq M_U / \gamma_R$$



γ_{dU} = partial safety factor reducing the whipping effect during collapse

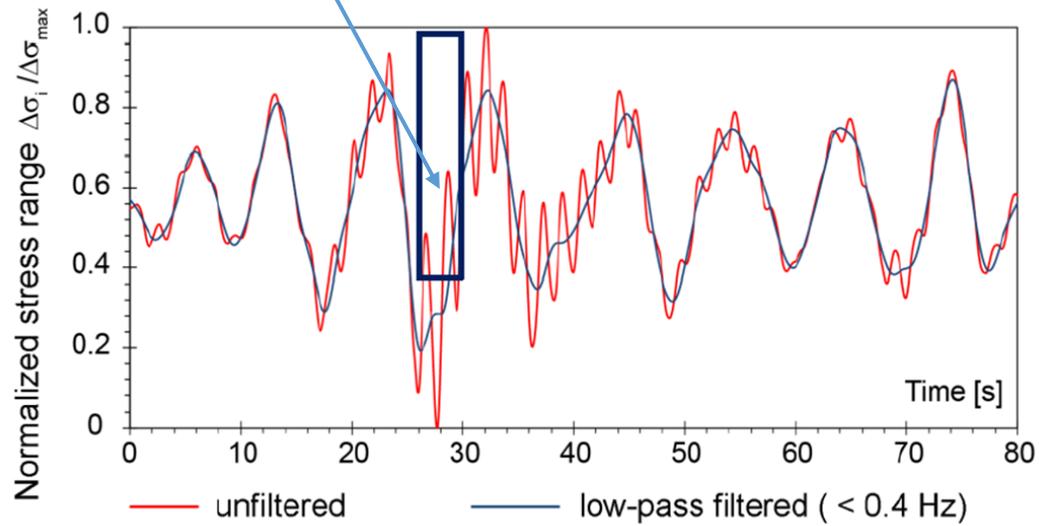
Whipping → transient hydro elastic ship structural response due to impulsive loading

→ by Large bow flare angle, high ship speed, low draft with flat bottom

→ structural failure of hull girder

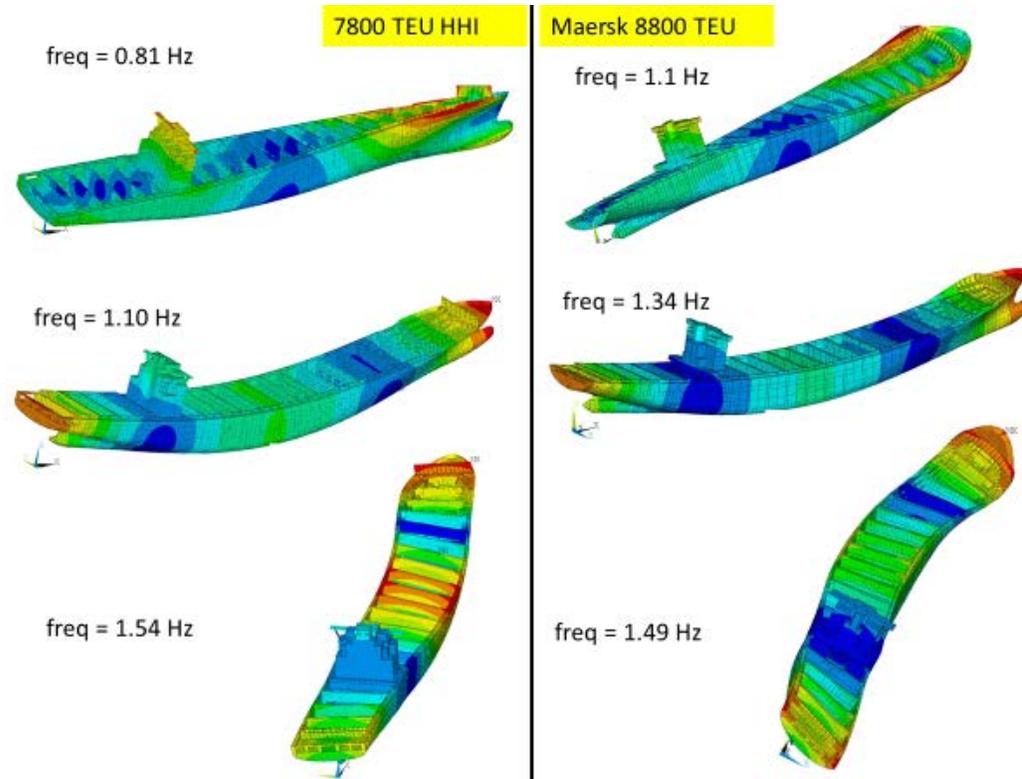
Collapse Modes of Container Ships

Frequency of 14000 TEU Container Ship
 0.54 Hz (1.85 sec)



Normalized Stress Range in Time Domain
 (Full Scale Measurement, DNV GL)

Frequency Modes of Container Ships



Solvers

Static Analysis → Implicit Solver [LS-DYNA]

$$K u(t) = F_{ext}(t) - F_{int}(t)$$

Dynamic Analysis → Explicit Solver [LS-DYNA]

$$M \ddot{u}(t) = F_{ext}(t) - F_{int}(t) - C \dot{u}(t)$$

Dynamic Analysis → Different times [0.1 sec, 1 sec, 2 sec, 5 sec, 10 sec]

- Without strain rate imposed by Cowper-Symonds constants
- With strain rate imposed by Cowper-Symonds constants

Cowper-Symonds Relation

Cowper-Symonds Equation:

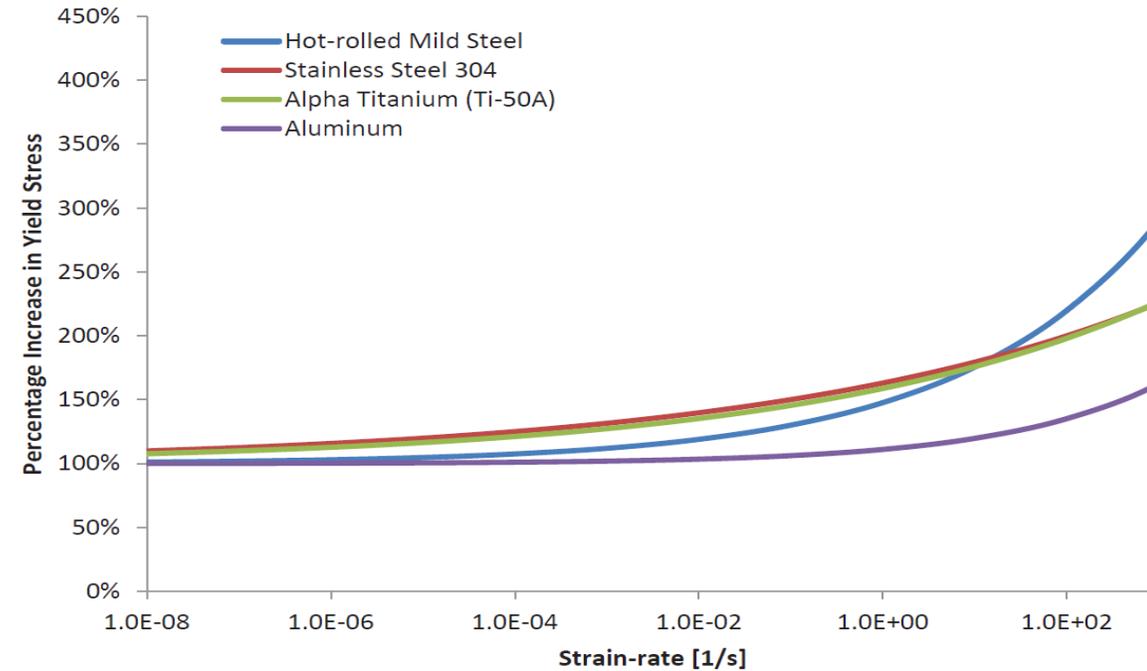
$$\sigma' = \sigma_y \left[1 + \left(\frac{\dot{\epsilon}}{C} \right)^{\frac{1}{p}} \right]$$

σ'_y = dynamic yield stress,

σ_o, σ_y = initial yield stress,

$\dot{\epsilon}$ = material strain rate,

C and p = Cowper-Symonds Constants



Behavior of Strain Rate(Experiments)

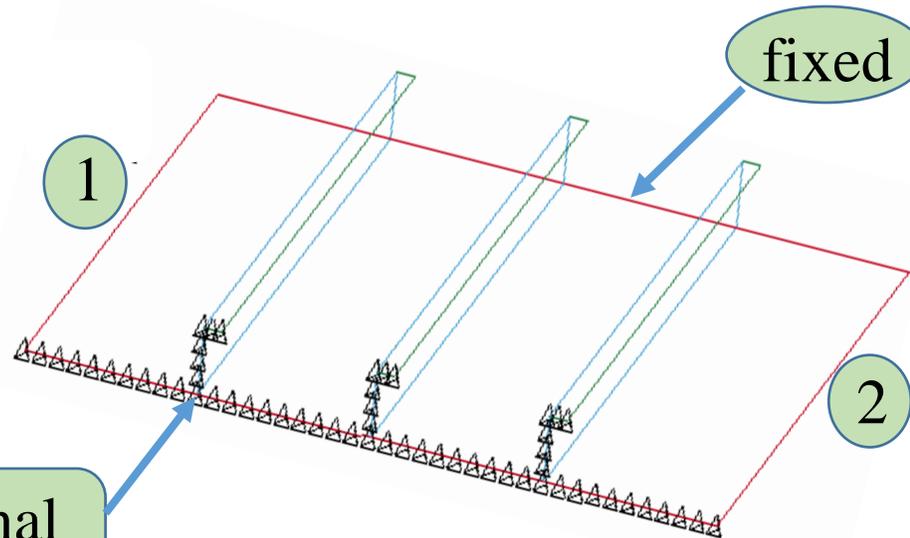
| Researchers' Name | Value of C | | Value of p | |
|-------------------------------------|--|--------------------|------------|--------------------|
| | Mild steel | High Tensile Steel | Mild steel | High Tensile Steel |
| Paik | 40.4 | 3200 | 5 | |
| Lim(2005) | 40 | 24086 | 5 | |
| Lim(2005) [for different steels] | $92000 \times \exp\left(\frac{\sigma_o}{364}\right) - 193779$ for $\sigma_o > 271\text{MPa}$ 40 for $\sigma_o \leq 271\text{MPa}$ | | 5 | |

Analyzed Models and Conditions

| Analyzed Model | Type of Steels Used in Model | Initial Yield Strength of Steel [MPa] | Analyzed Conditions | | |
|-----------------|------------------------------|---------------------------------------|---------------------|---------------------------------------|------------------------------------|
| | | | Static | Dynamic Condition without Strain Rate | Dynamic Condition with Strain Rate |
| Stiffened Panel | Mild Steel | 245 | Yes | Yes | Yes |
| | High Tensile Steel | 315 | Yes | Yes | Yes |
| Double bottom | High Tensile Steel | 315 | Yes | Yes | Yes |
| | Mixture of Steels | 235,315,355 | Yes | Yes | Yes |
| Cargo Hold | Mixture of Steels | 235,315,355, 390 & 460 | Yes | Yes | Yes |

Analysis of Stiffened Panel

Symmetric boundary condition at ① & ②



imposed translational displacement

- Stiffened Panel with Mild Steel
- Stiffened Panel with High Tensile Steel

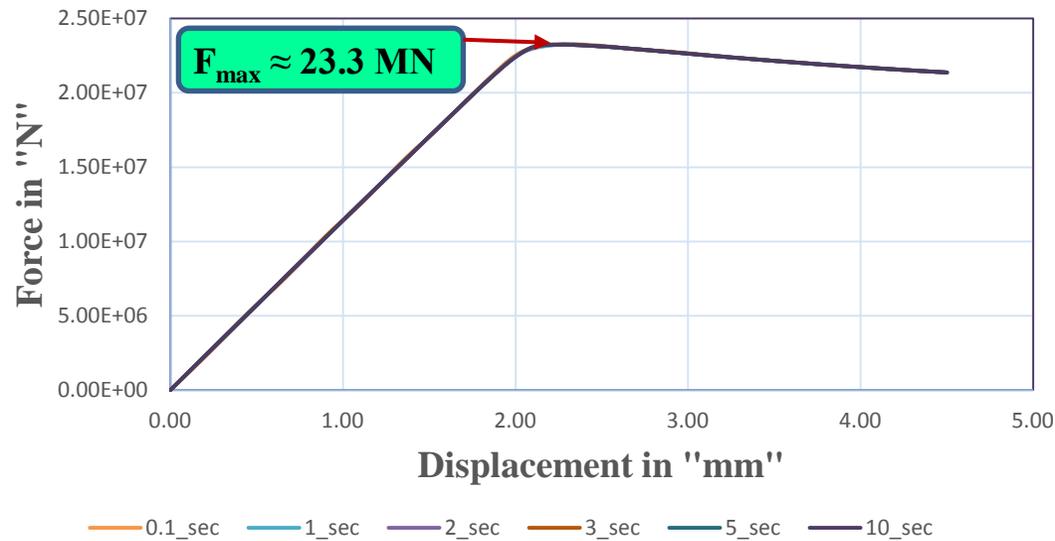


Impose the Strain Rate with Cowper-Symonds Constants recommended by **Lim & Paik**

Dynamic Analysis **without** Cowper-Symonds Strain rate

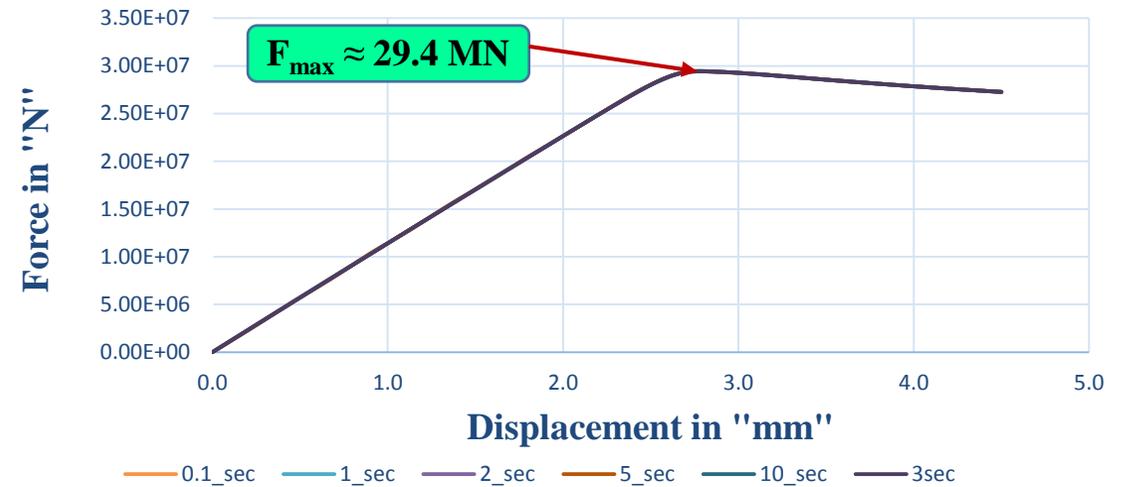
Static Collapse Force = 23.3 MN

Force Vs Displacement without Cowper-Symonds Strain Rate [Mild Steel]



Static Collapse Force = 29.38 MN

Force Vs Displacement without Cowper-Symonds Strain Rate [High Tensile Steel]



No significant changes in dynamic collapse compared to static collapse force

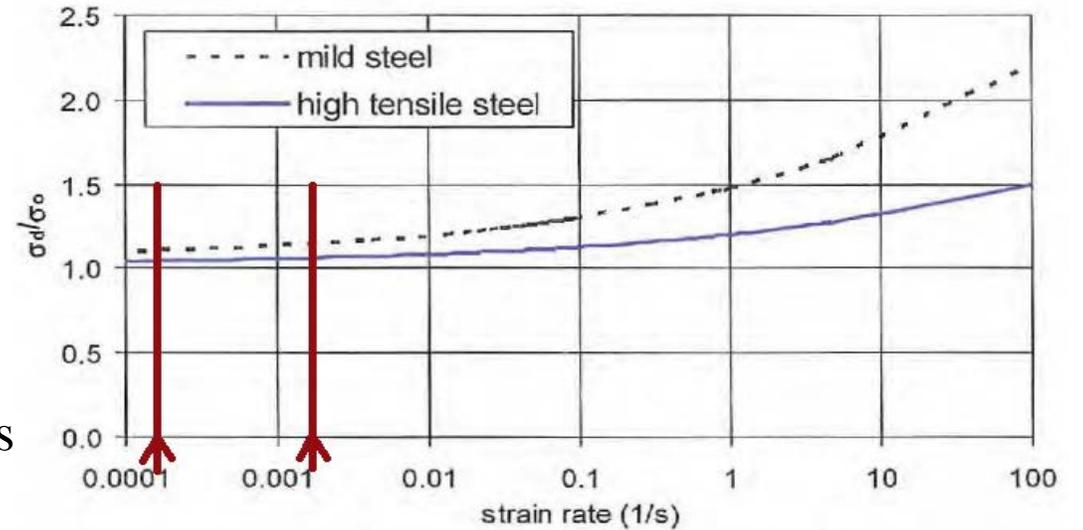
Dynamic Analysis **with** Cowper-Symonds Strain rate

| | Results with Mild Steel | | | Results with High Tensile Steel | | | | | |
|------------------------|-------------------------|-------------|-------------|---------------------------------|-------------|-------------|-------------------------|-------------|-------------|
| Static Collapse Force | 23.26 MN | | | 29.38 MN | | | | | |
| Researchers' Name | Lim & Paik | | | Lim | | | Paik | | |
| Simulation Time | Collapse Frequency [Hz] | Force Ratio | Strain Rate | Collapse Frequency [Hz] | Force Ratio | Strain Rate | Collapse Frequency [Hz] | Force Ratio | Strain Rate |
| 0.1sec | 15.38 | 1.29 | 2,46E-02 | 14.29 | 1.08 | 3.75E-02 | 14.29 | 1.12 | 2.66E-02 |
| 1sec | 1.67 | 1.21 | 2.77E-03 | 1.54 | 1.06 | 2.61E-03 | 1.43 | 1.09 | 2.66E-03 |
| 2sec | 0.80 | 1.19 | 1.26E-03 | 0.77 | 1.05 | 1.36E-03 | 0.74 | 1.08 | 1.32E-03 |
| 3.1sec,2.8 sec,2.8 sec | 0.54 | 1.17 | 8.10E-04 | 0.54 | 1.05 | 9.22E-04 | 0.54 | 1.07 | 9.45E-04 |
| 5sec | 0.33 | 1.16 | 5.68E-04 | 0.31 | 1.04 | 5.80E-04 | 0.30 | 1.07 | 5.10E-04 |
| 10sec | 0.17 | 1.14 | 2.66E-04 | 0.15 | 1.04 | 2.57E-04 | 0.15 | 1.06 | 2.54E-04 |

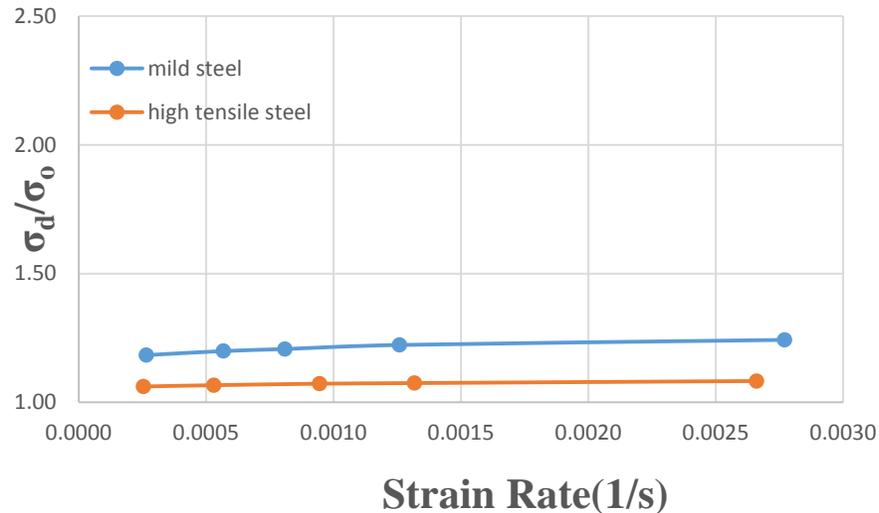
Validation of Strain Rate

Select C & P values recommended by **Lim**

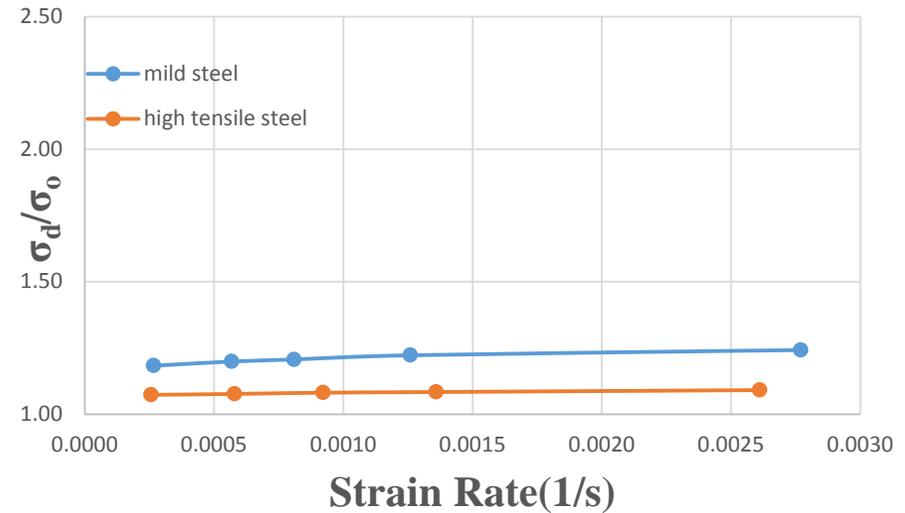
- Detail formulation for all type of ship structural steel
- Force increment ratio is less than that using Paik's constants
- Strain rate is also valid with the measurement values



Paik_Stress_Ratio Vs SR

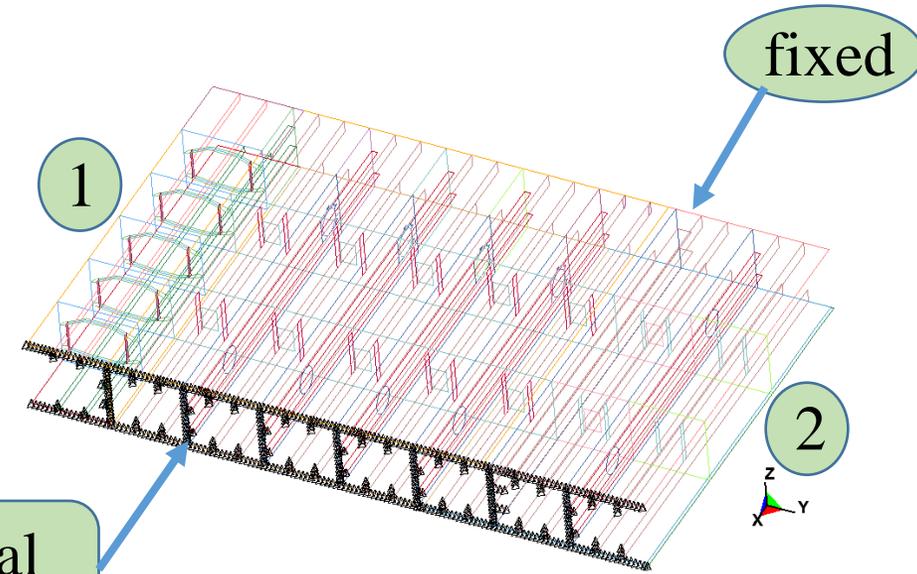


Lim_Stress_Ratio Vs SR



Analysis of Double Bottom Model

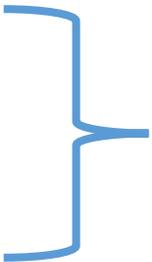
Symmetric boundary condition at ① & ②



Imposed translational displacement

Double Bottom Model with High Tensile Steel

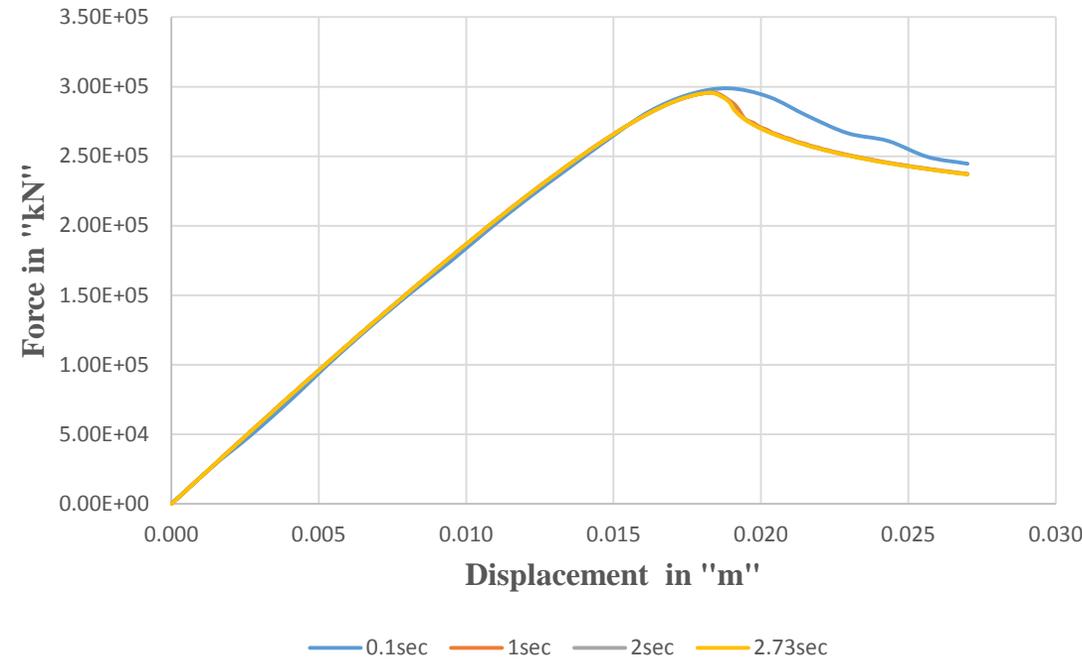
Double Bottom Model with Mixture of Steels
(235MPa, 315MPa and 355MPa)



Impose the Strain Rate with Cowper-Symonds Constants recommended by **Lim**

Dynamic Analysis **without** Cowper-Symonds Strain rate

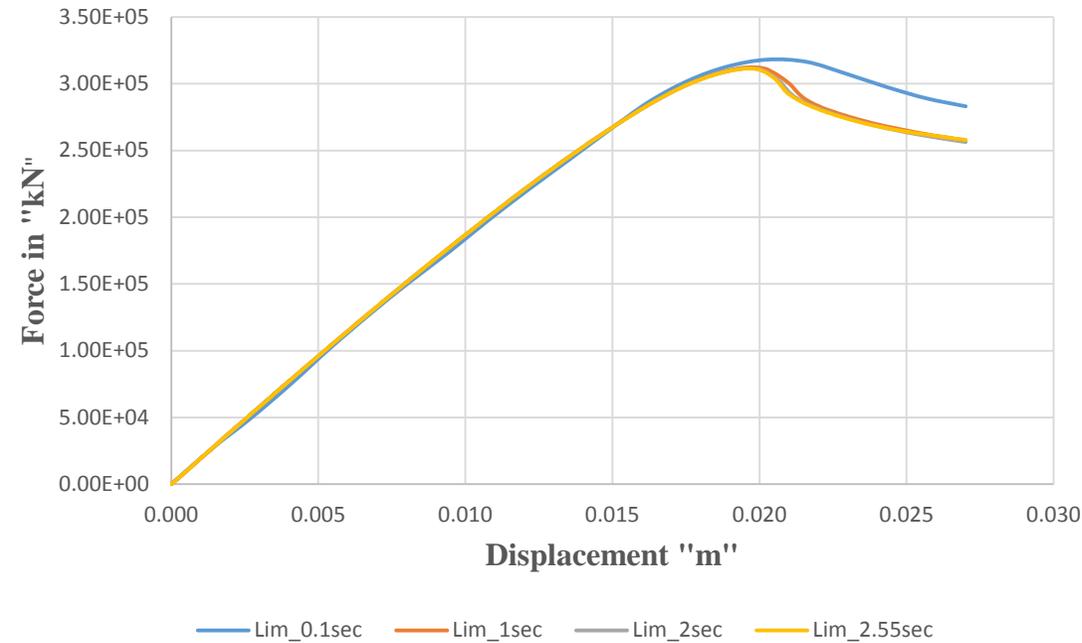
Force Vs Displacement without Cowper-Symonds Strain Rate [Mixture of Steels]



| | Results with High Tensile Steel | | Results with Mixture of Steels | |
|-----------------------|---------------------------------|-------------|--------------------------------|-------------|
| Static Collapse Force | 290.506 MN | | 295.40 MN | |
| Simulation Time | Collapse Frequency [Hz] | Force Ratio | Collapse Frequency [Hz] | Force Ratio |
| 0.1sec | 14.29 | 1.01 | 14.29 | 1.01 |
| 1sec | 1.52 | 1.00 | 1.47 | 1.00 |
| 2sec | 0.75 | 1.00 | 0.74 | 1.00 |
| 2.8sec, 2.73sec | 0.54 | 1.00 | 0.54 | 1.00 |
| 5sec | 0.30 | 1.00 | - | - |

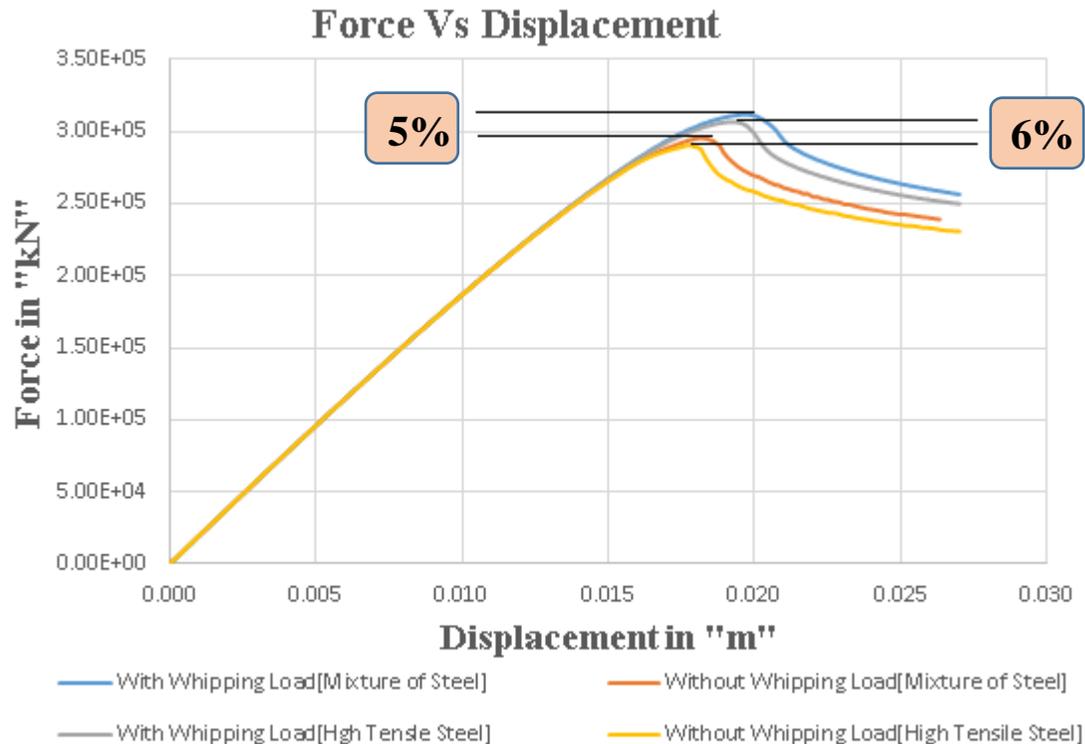
Dynamic Analysis with Cowper-Symonds Strain rate

Force Vs Displacement with Cowper-Symonds Strain Rate [Mixture of Steels]



| | Results with High Tensile Steel | | Results with Mixture of Steels | |
|------------------------------|---------------------------------|--------------------|--------------------------------|--------------------|
| Static Collapse Force | 290.51 MN | | 295.41 MN | |
| Simulation Time | Collapse Frequency [Hz] | Force Ratio | Collapse Frequency [Hz] | Force Ratio |
| 0.1sec | 13.33 | 1.08 | 13.33 | 1.08 |
| 1sec | 1.39 | 1.06 | 1.37 | 1.06 |
| 2sec | 0.70 | 1.06 | 0.69 | 1.05 |
| 2.59sec, 2.55sec | 0.54 | 1.06 | 0.54 | 1.05 |
| 5sec | 0.28 | 1.05 | - | - |

Comparison of the results of Double Bottom Model at 0.54 Hz

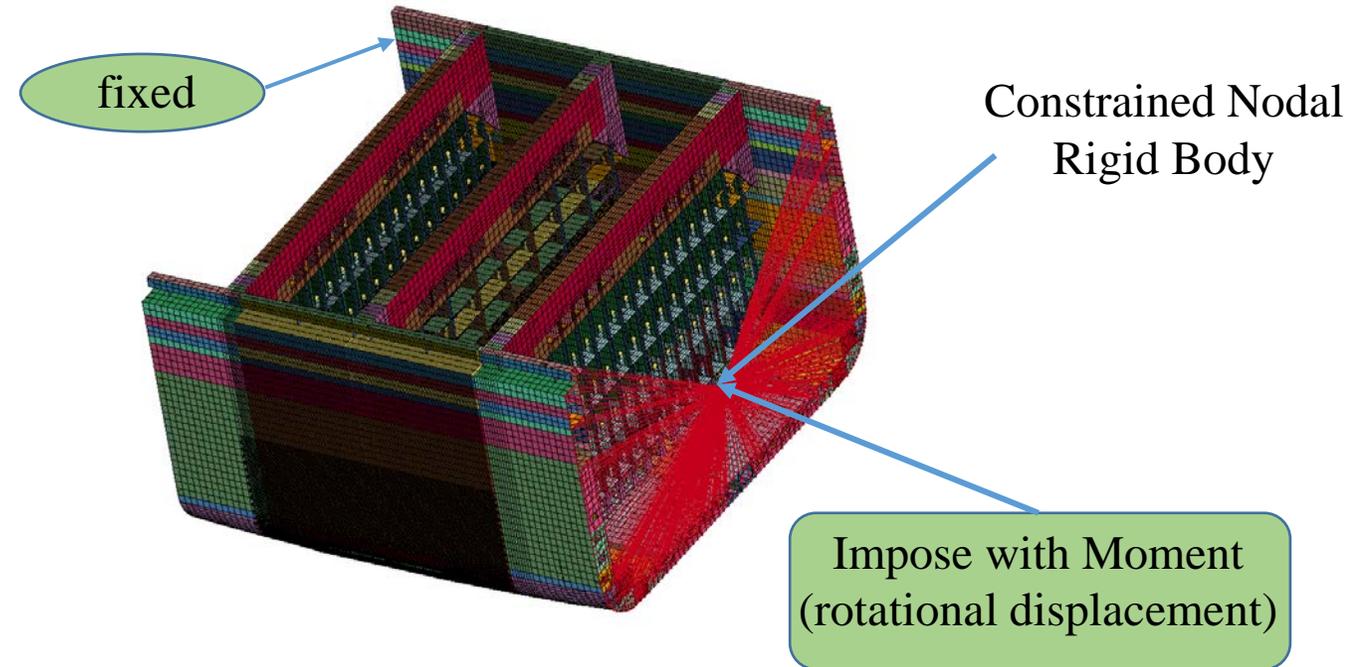


- **Without Whipping**
Mixture of Steels 2% greater than High Tensile Steel
- **With Whipping**
Mixture of Steels 2% greater than High Tensile Steel
- **Mixture of Steels**
With whipping 5% greater than without whipping
- **High Tensile Steel**
With whipping 6% greater than without whipping

Analysis of Cargo Hold Model

- Static Analysis
- Dynamic Analysis with Cowper-Symonds Strain Rate
 - Used Cowper-Symonds Constants recommended by **Lim**

| Materials in Model | Cowper-Symonds Constants | |
|--------------------------------------|--------------------------|---|
| | C | p |
| Initial Yield Strength of Steel[MPa] | | |
| 235 | 40 | 5 |
| 315 | 24806 | 5 |
| 355 | 50195 | 5 |
| 390 | 74819 | 5 |
| 460 | 131774 | 5 |



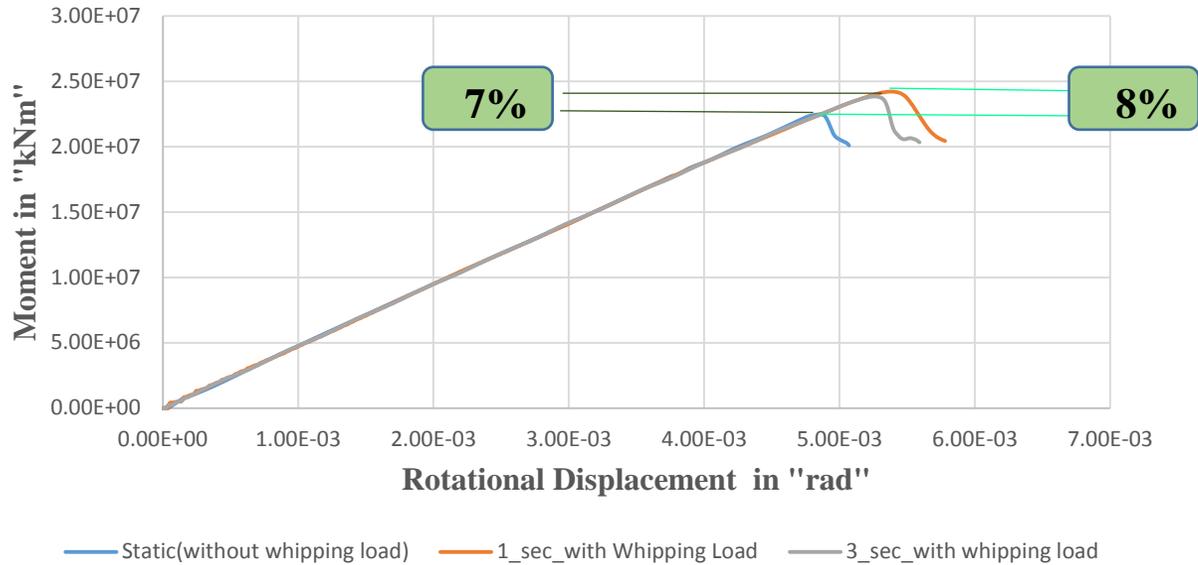
Dynamic Analysis of Cargo Hold Model

Static Collapse Moment = 22.38 GNm

| Simulation Time | Collapse Time [sec] | Collapse Frequency [Hz] | Dynamic Collapse Moment [GNm] | Moment Ratio | Strain Rate | Rotational Displacement [radian] |
|-----------------|---------------------|-------------------------|-------------------------------|--------------|-------------|----------------------------------|
| 1 sec | 0.54 | 1.86 | 24.21 | 1.08 | 1.83E-02 | 0.0054 |
| 3 sec | 1.68 | 0.59 | 23.84 | 1.07 | 5.03E-03 | 0.0053 |

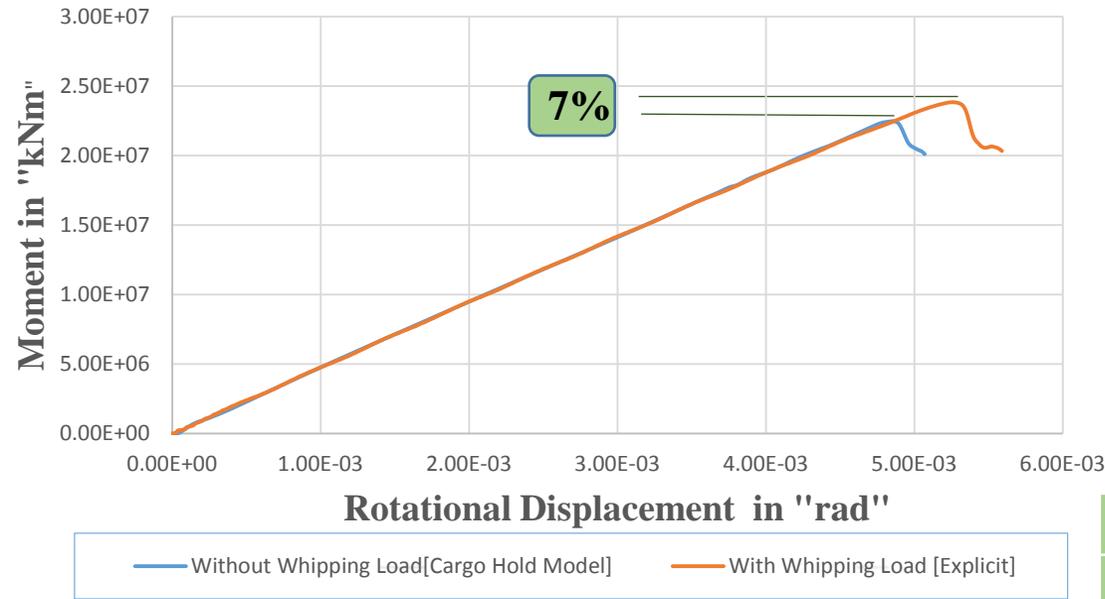
Desired Collapse Frequency of 0.54 Hz

Moment Vs Rotational Displacement



Hull Girder Ultimate Strength Check(14000 TEU Container Ship)

Moment Vs Rotational Displacement



$$\gamma_{dU} = 0.9 \text{ (DNV GL)}$$

$$\gamma_{dU} = 0.93 \text{ (Analysis)}$$

e.g. $M_{sw} = 8.5 \text{ GNm}$ and $M_{wv} = 8 \text{ GNm}$



| | DNV GL | Analysis | Unit |
|---|--------|----------|------|
| Load (with whipping) | 19.54 | 19.59 | GNm |
| Strength(with whipping) | 19.74 | 19.74 | GNm |
| UF (with whipping)[UF=load/strength] | 0.990 | 0.992 | - |
| Load(Static) | 18.10 | - | GNm |
| Strength(Static) | 18.53 | - | GNm |
| UF (Static)[UF=load/strength][w/o whipping] | 0.977 | - | - |

Conclusion and Recommendation

At Collapse Frequency of 0.54 Hz

| Analysed Model | Increment of Ultimate Strength Capacity due to whipping load including Strain Rate Effect | | |
|-----------------|---|--------------------|-------------------|
| | Mild steel | High Tensile Steel | Mixture of Steels |
| Stiffened Panel | 17% | 5% | - |
| Double Bottom | - | 6% | 5% |
| Cargo Hold | - | - | 7% |

- ❑ Ultimate Strength Capacity increases up to **7 %** (**10 %** by DNV GL)
- ❑ Simulation Time in LS-DYNA  a few days (sometimes, a few weeks)
- ❑ Need some implementation of FE Model

Thank You For Your Attention